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Thermomechanical study of polyethylene porous membrane by coating silicon dioxide nanoparticles

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Abstract: Polyethylene (PE) membrane has been extensively used in microtransport areas due to its high porosity, chemical stability, and easy processability. However, pure PE membrane shows poor thermomechanical properties. In this paper, silicon dioxide (SiO₂) was used to composite PE membrane in nanogel format. The morphology of the combination and surface layer was demonstrated by scanning electron microscopy (SEM) and atomic force microscopy (AFM). The SiO₂ gel on membrane was analyzed by Fourier transform infrared (FTIR), energy-dispersive X-ray spectroscopy (EDX), and X-ray diffraction (XRD). The effect of the SiO₂ gel on the thermomechanical properties of PE membrane was investigated in terms of thermal shrinkage, thermogravimetric analysis (TGA), and dynamic mechanical analysis (DMA). The results showed that the SiO₂ gel effectively reduced the thermal shrinkage of PE membrane by 47.25% without increased crystallinity, and the coating layer slowed down the decomposed speed of PE membrane at melting point. Comparison tests showed that SiO, gel enlarged the storage modulus and Young's modulus of PE membrane. Tensile test revealed that the maximum load on pure PE and PE composite membranes at the yield point were both decreased with the increased temperature.

Keywords: polyethylene; silicon dioxide; sol-gel coating; thermomechanical property.

1 Introduction

Polyethylene (PE) membrane, a kind of porous thin film with countless microfibrils after dry or wet double stretching in manufacture, has been widely used in industrial applications related to ion and fluid transfer areas [1–5]. Pure PE membrane shows high chemical stability, superhydrophobicity, and relatively stable porous structure [6–8]. However, the low temperatures of glass transition and melting of PE imply that the ion/fluid transfer can enhance the mobility of macromolecules and then disorder the alignment of molecular chains beyond a critical temperature value after the heat accumulation at the interface. This is shown as the thermal shrinkage of PE membrane [9], which is regarded as the great safety concern of PE membrane in use, especially when it works as a PE separator in battery [10, 11].

The combination with a kind of high melting point material can enhance the thermal safety of PE products [10, 12, 13]. The sol-gel coating process describes an effective way in combining the low melting temperature polymer with high melting point inorganics [14]. The process relates to a transition of a chemical solution in colloidal into an integrated network in a solid porous structure. The precursors used mostly in sol preparation are normally inorganic salts or metal organic compounds, such as metal alkoxide. The precursor is subject to a series of hydrolysis and polymerization reactions to become a colloidal suspension, namely, a sol. The liquid sol components can penetrate into the porous structural PE membrane and adhere to the surface of microfibrils. The sol then evolves towards an inorganic network containing a liquid gel phase due to the crosslinking of inorganic or organic compounds. The drying of the gel can remove the liquid phase, causing the formation of a porous structural material in and upon the PE membrane. In recent years, the sol-gel coating process has been used increasingly to introduce some functional matter on various forms of materials, such as steel [15], glass [16], and polymers [17].

In this article, we coated PE porous membrane with silicon dioxide (SiO₂) gel using a dipping \rightarrow coating \rightarrow drying

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approach. The surface morphology of the coated membrane was demonstrated by scanning electron microscopy (SEM) and atomic force microscopy (AFM). Fourier transform infrared (FTIR) and energy-dispersive X-ray spectroscopy (EDX) were used to analyze the composite structure of PE/SiO₂ gel. The effect of SiO₂ gel on PE thermomechanical properties was studied using flame-close reaction, thermogravimetric analysis (TGA), dynamic mechanical analysis (DMA), and temperature rise in stretching.

2 Materials and methods

2.1 Materials

A roll of PE membrane (with thickness of 8 μ m) was used in this study. The membrane samples were all first washed in ethanol (EtOH) followed by two rinses in distilled water and then were dried at 40°C in an oven.

2.2 Preparation of SiO, sol

The SiO₂ sol was prepared by mixing precursors tetraethyl orthosilicate (TEOS; CAS:78-10-4) and EtOH (98%) at room temperature with high-speed stirring. HCl was then added into the mixture as a catalyst followed by deionized water and dimethylformamide (DMF), which were mixed into the system as buffers. The five liquid materials were mixed at a molar ratio of 1:8:0.04:3:1.6 (TEOS/EtOH/HCl/ H₂O/DMF), and the reaction formula is as follows:

$$Si(OC_2H_3) + 4H_2O = Si(OH)_4 + 4C_2H_3OH$$
 (1)

$$\begin{array}{ccc} OH & OH & OH & OH \\ HO-Si-OH + & HO-Si-OH \longrightarrow & HO-Si-OSi-OH + H_2O & (2) \\ OH & OH & OH & OH \end{array}$$

Formula (1) is the hydrolysis reaction using the HCl catalyst, and Formula (2) is the condensation of the hydrolysis products. The two-step reactions were going at the same time. The preparation of SiO_2 was carried out for approximately 6 h at 30°C with high-speed stirring. A kind of stable, thick, transparent liquid sol was then formed after the reaction.

2.3 Sol-gel coating on membrane

The samples of PE membrane were immersed in the asprepared sol for 30 min. The wet PE membranes were then rolled on a very smooth surface plate by a glass bar. These steps were repeated twice. The extra liquid on the sample surface was absorbed by paper tissue. The membrane samples were then dried in an oven at 40°C for 1 h. The working principle is shown in Figure 1.

2.4 Surface characterization

2.4.1 SEM and AFM characterization

The surface morphology of PE and PE/SiO₂ gel membranes were observed using SEM (JEOL Model JSM-6490). EDX (JEOL Model Oxford INCA Energy 250) was used for chemical element confirmation. AFM (CSPM4000; Benyuan Company) was employed to measure the dimensions of dried gel particles, where the tapping mode was used. All samples under SEM observation were scanned at room temperature in nitrogen, whereas samples under AFM were scanned at ambient atmosphere.

2.4.2 FTIR and X-ray diffraction (XRD) analysis

The chemical functional groups of PE and PE/SiO₂ gel membranes were examined by FTIR spectroscopy (Perkin-Elmer Spectrum 100 FTIR Spectrometer, USA) in the range of 4000–650 cm⁻¹ using attenuated total reflectance (ATR)-Ge method. The absorption spectra were recorded with 64 scans with a resolution of 16 cm⁻¹. The crystallinity of PE and PE/SiO₂ gel membranes was measured by XRD (Rigaku SmartLab 9KW XRD System) with 2 θ values from 15° to 30° and recorded at a scan speed of 3° min⁻¹ at 40 kV and 40 mA, which was equipped with Cu K α radiation with a wavelength of 1.54 Å.



Figure 1: Schematic illustration of SiO₂ sol preparation and PE membrane by sol-gel coating.

2.5 Thermomechanical investigation

2.5.1 Thermal shrinkage

For comparison of thermal stability, PE and PE/SiO_2 gel membranes were implemented as follows: (a) the burning behavior was achieved close to the alcohol burner and recorded by the camera and (b) the membrane samples were heated in vacuum oven from room temperature to 120°C with a heating rise rate of 5°C min⁻¹ and maintained at 120°C for 15 min. The thermal stability of the composite membranes was expressed by variation of the membrane size. The larger change of membrane size means poorer thermal stability under high temperature.

2.5.2 Thermomechanical analysis

The thermomechanical performance of PE and PE/SiO₂ gel membranes was studied by TGA (Mettler Toledo TGA/DSC-1 Thermal-Analyser, Switzerland), DMA (Perkin-Elmer Diamond, DMA, USA), and Instron-5566 universal test machine with a heat chamber (Instron Calibration Lab, 5566Q7582). The investigations of samples by TGA, DMA, and Instron-5566 were all using nitrogen as purge gas, and temperature parameters were set from 20°C to 700°C with a heating rate of 10°C min⁴, from 20°C to 150°C with a heating rate of 2°C min⁴, and from 30°C to 120°C (30°C, 60°C, 90°C, and 120°C) with an elongation rate of 10 mm min⁴, respectively.

3 Results and discussion

3.1 Analysis of thermal stability

As is known, the thermoplastic polymer has a nature of shrinking and melting when close to fire flame. This is owing to the enhanced mobility of long macromolecular chains and increased entropy for the unstable orientation of molecules under heat accumulation [18]. This shrinkage is obviously illustrated as shown in Figure 2A with black curly bead close to flame. Comparably, solid integrated SiO₂ gel blocks the curly shrinking of membrane, which fires directly after heat accumulation to the PE decomposed temperature shortly. Quantitatively, two 2×2 cm square frames were marked on the surface of two kinds of membranes, and then the membranes were heated up to 120° C under vacuum for 30 min. The two membranes experienced different size declines as the temperature increases, as shown in Figure 2B. Figure 2C shows that the area of marked frame

on the PE membrane decreases from 4 to 1.77 cm^2 (44.25%), and the area of 3.66 cm² (91.5%) for shrinked PE/SiO₂ gel membrane under 120°C, indicating the significant improvement of thermal stability of PE membrane when coated with SiO₂ gel. The larger error bar of PE shrinkage variation discloses the uneven porous structure of PE membrane, which causes the anisotropic shrinkage under heating, whereas the filled solid SiO₂ gel prevents the anisotropic shrinkage of PE membrane significantly.

3.2 SEM, EDX, and AFM characterization

Figure 3A and B shows the surface morphology of PE and PE/SiO₂ gel composite membranes, where PE shows a porous structure due to the liquid-solid phase separation during membrane manufacture, and PE composite membrane displays a smooth surface of SiO, gel layer. The SiO, gel layer was analyzed by EDX with a point spectrum for confirming the Si-element existence (Figure 3D). AFM images (Figure 3C and D) show that the SiO, gel layer of PE membrane consists of gel nanoparticles with diameters from 5 to 50 nm using cross-section analysis for an arbitrary blue line. This diameter range of nanoparticles can definitely penetrate into the internal pores among microfibrils as shown in Figure 3A. However, it is noted that the densely stacked nanoparticles may not contribute to the modification of PE membrane when applied to battery separators as the significant decrease of membrane porosity. The effect of densely coated SiO, nanoparticles on PE membrane porosity was consistent with Jeong and Lee's work [19].

3.3 FTIR, XRD, and TGA analysis

In the XRD characterization of PE and PE/SiO₂ gel membranes (Figure 4A), characteristic peaks can be identified at 21.6° and 24.2° of 2θ . The sample crystallinity obtained from XRD was approximately 40% for PE and 15% for PE/SiO₂ gel membranes according to Eq. (3) [20]:

$$Xc = \frac{A_{\rm T} - A_{\rm A}}{A_{\rm T}}$$
(3)

where $A_{\rm T}$ denotes the total area of the diffractogram and $A_{\rm A}$ denotes the area corresponding to the amorphous region. Thus, it is inferred that no crystalline phase exists inside the SiO₂ gel after coating based on the same abscissas of peaks of the two scanned curves.

The effect of coated SiO_2 gel on PE membrane was analyzed by FTIR, as presented in Figure 4B. The high



Figure 2: Thermal stability of PE membranes and PE/SiO₂ gel composites: (A) comparison of close-to-flame reactions; (B) and (C) area variation of both membranes under 20°C and 120°C.

peaks from 720 to 2916 cm⁴ demonstrated organic signals, such as a characteristic spectra of the asymmetric stretching vibration band of \perp -C-C- at the peak of 2916 cm⁴ and symmetric stretching vibration band of \parallel -C-C- at the peak of 2850 cm⁴. The peaks at 1461 and 723 cm⁴ indicated the existence of symmetrical curve vibration of \perp -C-C- at the PE crystal area and out-of-plane twist vibration of \perp -C-Cand *b*-axis of CH₂ at the PE crystal areas. The characteristic peaks at 1651, 1066, and 973 cm⁴ represent the H-OH curve stretching vibration, the Si-OH curve vibration, and the Si-O-Si asymmetric/symmetric stretching vibrations, respectively. These peaks prove the SiO₂ gel on the PE membrane.

Figure 4C shows the measured weight percentage of PE and PE/SiO₂ gel membranes in the temperature range from 25°C to 700°C. It is noted that PE membrane shows weight balance until its decomposed temperature at 475°C, and the weight drops dramatically from this temperature. This is attributed to the porous structure

and orientation disordering of PE macromolecular chains at decomposition and evaporation. However, the TGA curve of PE/SiO_2 gel membrane presents a slowly weight decrease with the increase of temperature and a dramatic weight drop at the same decomposed temperature of PE membrane, following with an almost constant line (residual weight) in the test temperature range. The slow reduction of weight indicates that the gel still contains sol-phase "liquid", which is locked inside the gel network and escapes at high temperature. The final residual 60% of weight is composed of SiO₂ nanoparticles, which are not able to decompose in the test range of temperature.

3.4 Analysis of thermostretching properties

Figure 5 compares the surface morphologies of PE and PE/ SiO₂ gel membranes under stretching at 120°C. There are a



Figure 3: SEM images of (A) PE membrane and (B) PE/SiO₂ composite membrane and EDX observation of Si element on PE membrane and AFM images of (C) SiO₂ gel nanoparticles, (D) confirmation of Si element deposited on the PE membrane and (E) SiO₂ gel particle dimension distribution.



Figure 4: Testing results of PE membrane and PE/SiO, gel composites from (A) XRD, (B) FTIR, and (C) TGA.

number of white lines in parallel alignment on the surface of pure PE membrane, which is attributed to the reorientation of -C-C- molecular chains under large elongation at high temperature. These white lines are covered by SiO₂ gel particles on the PE/SiO_2 gel membrane, which displays slight extrusion tendency of SiO_2 gel particles as shown in the red arrows in Figure 5, indicating the resistance of SiO_2 gel to the PE thermostretching behavior.



Figure 5: SEM images of PE membrane and PE/SiO, gel composites under stretching at 120°C.

Figure 6 gives the results of DMA tests regarding the storage modulus (E') and phase angle (D), which are the function of temperature (T) for the two membranes. Two plateaus appear as the glass- and rubbery-like states in Figure 6A, and the storage modulus reduces abruptly at 128°C for the PE and at 144°C for the PE/SiO₂ gel membranes, indicating that the coated SiO₂ gel can enhance the glass transition temperature and the modulus of PE porous membrane to some extent. Oppositely, the phase angle reflects the ratio of the viscous portion to the elastic portion of a polymer. The angle of PE membrane is observed larger than that of the PE/SiO₂ gel membrane from Figure 6B. This implies a good thermal protection of SiO, gel in preventing PE macromolecular chains from flowing above the glass transition temperature, owing to the stable thermal performance of SiO₂ gel nanoparticles in the porous PE membrane.

During the Instron-5566 tensile tests, each sample dimension is a rectangle of 2.5×5 cm, and each one was performed under a series of constant temperatures. It is found that the maximum yield loads of both membranes decrease as the temperature increases from P30/PS30 (30°C) to P120/PS120 (120°C). The initial Young's moduli of the tested membrane (slope of curve) have the same tendency along the increasing temperature, as shown in the histograms in Figure 7. The membrane strain achieves a higher value at the maximum yield load under a higher temperature as shown in the curves in Figure 7, owing to the increased mobility of macromolecular chains and less crystallinity of the membrane. The coated SiO₂ gel nanoparticles improve the Young's modulus of membrane significantly by two times higher than the pristine value, indicating the sufficient enlarged stiffness of the modified membrane. This is coincident with the enlarged storage modulus of PE/SiO₂ gel composite membrane from the DMA test.

4 Conclusions

This work investigates the effect of coated SiO₂ gel on the thermomechanical properties of porous PE membrane. The SEM and EDX observations reveal the porous structure of PE membrane with dimension in nanoscale of pores and combination of SiO₂ gel nanoparticles on the membrane surface. The dimensions of particles are also measured by AFM. FTIR and XRD measurements disclose the existence



Figure 6: DMA of PE membrane and PE/SiO_2 gel composites along heating duration.



Figure 7: Thermotensile of membrane composites by Instron under 30°C, 60°C, 90°C, and 120°C.

of Si-O and C-C bonds in the PE/SiO₂ gel composite and decreased crystallinity by coated SiO₂ gel. TGA test shows the slow decomposition of SiO₂ gel for phase separation until the fully decomposed of PE membrane, indicating the net structure of gel in porous PE membrane. It is experimentally found that the coated SiO₂ gel can prevent the PE membrane from thermal shrinkage significantly under the temperature of 120°C, and the gel improves the membrane storage modulus, Young's modulus remarkably with the increased stiffness. The maximum load at yield and the modulus are both decreased with the increase of test temperature, and the gel has slight effect on the trend, indicating that the sol-gel coating has a slight effect on the

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References

 Bleha M, Kudela V, Rosova EY, Polotskaya GA, Kozlov AG, Elyashevich GK. *Eur. Polym. J.* 1999, 35, 613–620. [2] Arora P, Zhang ZJ. Chem. Rev. 2004, 104, 4419-4462.

- [3] Sohn JY, Gwon SJ, Choi JH, Shin J, Nho YC. *Nucl. Instrum. Methods Phys. Res. B* 2008, 266, 4994–5000.
- [4] Huang X. J. Solid State Electrochem. 2011, 15, 649-662.
- [5] Guan HY, Lian F, Ren Y, Wen Y, Pan XR, Sun JL. Int. J. Miner. Metallurg. Mater. 2013, 20, 598–603.
- [6] Zhang C, Bai Y, Sun Y, Gu J, Xu Y. J. Membr. Sci. 2010, 365, 216–224.
- [7] Schauer J, Brozova L. J. Membr. Sci. 2005, 250, 151–157.
- [8] Gupta B, Anjum N. J. Appl. Polym. Sci. 2001, 82, 2629–2635.
- [9] Zhang SS. J. Power Sources 2007, 164, 351-364.
- [10] Choi JA, Kim SH, Kim DW. J. Power Sources 2010, 195, 6192-6196.
- [11] Kang SM, Ryou MH, Choi JW, Lee H. Chem. Mater. 2012, 24, 3481–3485.
- [12] Xiao X, Long A. Sci. Eng. Compos. Mater. 2014, 21, 99–109.
- [13] Umberto P. Sci. Eng. Compos. Mater. 2014, 21, 197–204.
- [14] Xiao X, Chen F, Wei Q, Wu N. J. Coat. Technol. Res. 2009, 6, 537–541.
- [15] Checmanowski JG, Szczygieł B. J. Non-Cryst. Solids 2008, 354, 1786–1795.
- [16] Zhao X, Zhao Q, Yu J, Liu B. J. Non-Cryst. Solids 2008, 354, 1424–1430.
- [17] Bessiere A, Badot JC, Certiat MC, Livage J, Lucas V, Baffier N. Electrochim. Acta 2001, 46, 2251–2256.
- [18] Woo JJ, Nam SH, Seo SJ, Yun SH, Kim WB, Xu T, Moon SH. Electrochem. Commun. 2013, 35, 68–71.
- [19] Jeong HS, Lee SY. J. Power Sources 2011, 196, 6716–6722.
- [20] Poley LH, Siqueira APL, da Silva MG, Vargas H. Polimeros Cienc. Tecnol. 2004, 14, 8–12.